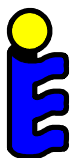


**Internal procedures for Solar Keymark WP1.A
and input to CEN/TC 312**

**Version: 1
2002-10-16**

Edited by:
Åsa Wahlström
SP Swedish National Testing and Research Institute

Solar Keymark
WP1.A
Network for implementing standards
Solar Collectors



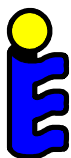
Internal procedures for Solar Keymark WP1.A and input to CEN/TC 312

During the Solar Keymark project comments of the EN12975-1&2 (solar collectors) have been collected and frequently discussed by emails and during the meetings. The main aim with collecting the comments has been to help each other in implementing test procedures for Solar Keymark labelling, to identify difficulties with performing the tests and to interpret the harmonised standards. Some of the most useful comments that have facilitated the implementations of the test procedures and accreditations have been collected in this document. This document primarily aims to act as Solar Keymark internal procedures for the operational procedure of performing the tests and secondly gives suggestions for revision of the standards to the CEN/TC 312 for the next scheduled revision of the harmonised standards.

This is the first version of this document and it is aimed for discussions and acceptance in the 4th Solar Keymark meeting in Rome. Additional comments, which were addressed at the 3rd Solar Keymark meeting in Vienna for further investigations, will also be discussed at the Rome meeting. These additional comments will be added to this document after the meeting in order to make a final version for the 5th Solar Keymark meeting in Portugal. The additional comments will primarily be:

- Recommendations on how to structure the standard better for the quasi-dynamic test in order to help the laboratories to make better selections of data points for parameter identification.
Action from: Peter Kovacs
- Calibrating pyranometers
Action from: Åsa Wahlström and Carmen Granados Casals
- Mechanical load test
Action from: Pierre Richard and Åsa Wahlström
- Uncertainty of test result
Action from: Pierre Richard and Ueli Frei (through Åsa Wahlström)
- Clause 6.3.5.2
Action: Hubert Fechner
- Inconsistence between 12975-1 and 12975-2
Action: Hoang Liuwaw and Åsa Wahlström

See WP1.A minutes from previous Solar Keymark meetings for further information about the addressed problems in these comments.



Comments to EN 12975-1

Comment 1: *Change prEN to EN*

The standard is referring to prEN 12975 instead of EN 12975, throughout the complete document.

Comments to EN 12975-2

Comment 1: *Better structure, layout and table of contents*

The standard is not well structured. Required conditions (figures etc.) are often not in a table. This makes it not easy to work with. Also the chapters could be better structured, for instance a new chapter on a new page etc. It's impossible to find something by using the table of contents. The table of contents should include all chapters, from main chapter 1-6 with sub chapters e.g. 6.1.1.1.

Comment 2: *Mix up of "Uncertainty" and "Accuracy"*

The word accuracy is often used when it supposed to be uncertainty. For example in 6.1.2.3.2.1.

Comment 3: *Specify properties of coating*

The documentation of test results requires only the name of the material of the absorber coating (given in Annex D.2 and Annex F.2). This makes it difficult to identify the material. It would be beneficial if it is required that the manufacturer must give values for α and ϵ for documentation of the coating.

Comment 4: *Symbols and units, page 5:*

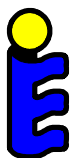
Coefficient b_0 for the incidence angle modifier $K_{\Theta b}$ is missing

Comment 5: *Second method of identification of parameters in QDT*

Beside the Multiple Linear Regression (MLR) for identification of parameter values in the QDT equation (in 6.3.4.8.1) also other methods should be possible to use. For example algorithms for non-linear models as the Levenberg-Marquart-Algorithm and the DF-program as used for Dynamic System Testing acc. to ISO 9459, Part 5. The work within IEA SH&C Task XIV has showed that both approaches lead to the same results. The advantage of MLR is the simplicity of the data evaluation, whereas the non-linear model is more flexible with respect to special collector designs. Solar Keymark suggest that Work group 1 (CEN/TC 312) should investigate if the suggested methods lead to the same result. This could be verified in an inter-comparison of test results of QDT measurements. The verification will tell if the methods should be taken into account for the revision of the standard.

Comment 6: *Heading Annex D and Annex F*

The heading in Annex D and F should be without "... under steady state conditions" since the "performance test reports" are also for reporting tests done according to the quasi dynamic method.



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Comment 7: Annex E

The symbol η_0 has become a square in table "Based on Absorber Area" and table "Based on Aperture Area" in Annex E. Should be changed. (The same in Annex G.)

It should be clearer if it is mentioned that 6.1 is the steady state method and 6.3 the quasi-dynamic method under "Thermal performance has been tested based on the test methods" in Annex E (as it is done in Annex F)

6.1 Outdoor (steady state) ☐ 6.1 Indoor (steady state) ☐ 6.3 Outdoor(quasi-dynamic) ☐

In the table "Power Output per collector unit (W)" in Annex E it should be indicated that these values are for normal incidence

Comment 8: Annex M

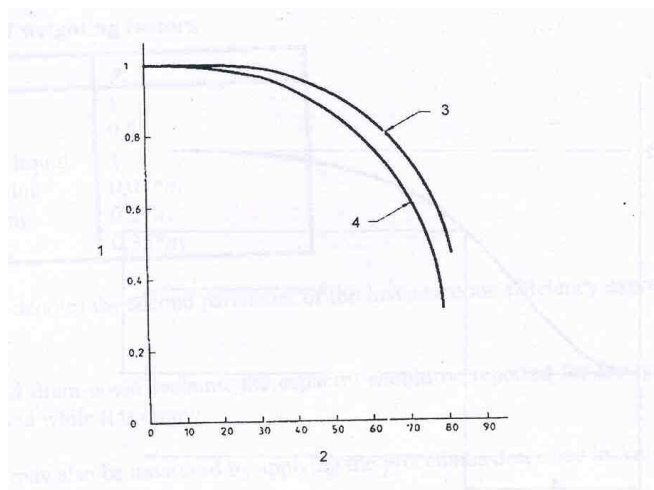
In the standard Annex M is only informative. In Annex G, that is normative, it is stated that if thermal performance has been tested according to 6.3, test results according to Annex M should be attached. Therefore Annex M should be normative in case of testing according to 6.3

Comment 9: Table number

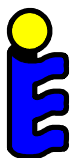
In 6.1.5.2. should the reference to table 1 should be table 5.

Comment 10: Illustrations

In 6.1.7.1 the Figure 5 is wrong figure and should be the one showed below.



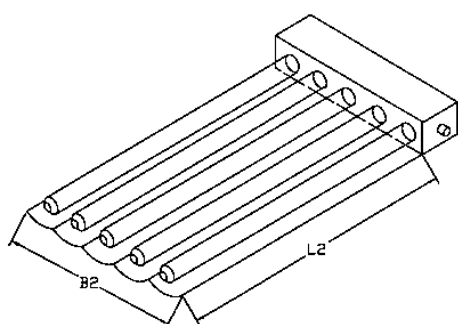
Right Figure 5



Comment 11: Illustrations

In Annex I the Figure I.3 is wrong figure and should be the one showed below.

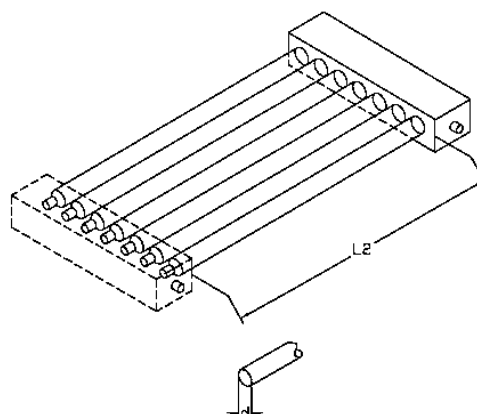
Aperture Area of Tubular Collector



$$A_a = L_2 \times B_2$$

Tubular Collector with Reflector
Length: L_2 ; Length of exposed reflector.
Width: B_2 ; Width of exposed reflector.

Figure I.3

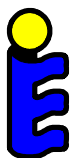


$$A_a = L_2 \times d \times N$$

Tubular Collector without Reflector
 d : Internal Diameter
 L_2 : Length of Parallel and
Transparent Section of the Tube.
(Length of Absorber)
 N : Number of Tubes.

Figure I.4

Right Figure I.3

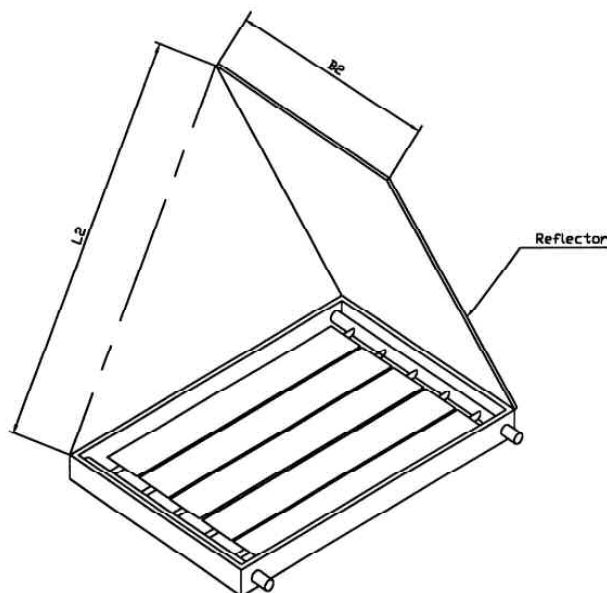


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Comment 12: Illustrations

In Annex I the Figure I.5 is wrong figure and should be the one showed below.

Aperature Area of Flat Plate Collector



$$A_a = L_2 \times B_2$$

Figure I.5

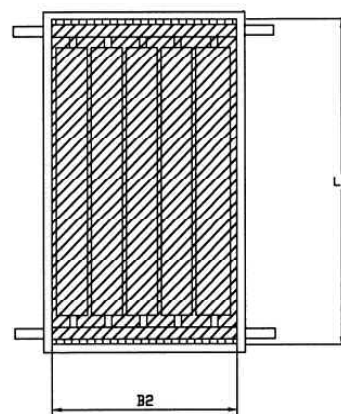


Figure I.6

Right Figure I.5

Comment 11: Maximum T_m^* values

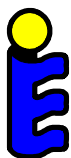
In 6.1.4.4 it says that the maximum temperature shall be at least around 80 °C. This should be changed to “shall be chosen so that maximum T_m^* value is at least 0.09 unless the temperature difference become smaller than required in 6.1.4.3.”

Comment 12: Choice of absorber test

Four different methods are described for heating the absorber in clauses 5.2.2.2.2 through 5.2.2.2.4. In Annex B.13.2.2, page 96, it should be written which method that has been used. It is not clear which method that should be used under certain conditions or if it is a free choice. Add at the end of 5.2.2.1 “One of the methods described in 5.2.2.2.2 through 5.2.2.2.4 may be chosen.

Comment 13: Clarification

Add at the end of 6.2.4.8.1 “NOTE: Positive EL values are a downward oriented irradiance onto a surface with a temperature of 0 K.



Comment 14: *Delete per square meter two times*

One can not calculate a value “per square meter” without knowing the reference area to use. Furthermore the effective thermal capacity of collector, C , has the unit (JK^{-1}) and the specific heat capacity, c_i , has the unit ($\text{Jkg}^{-1}\text{K}^{-1}$) according to page 5 and 6.2.6.2. Therefore, must the mass, m_i , in Equation 29 has the unit kg (that is in consistence with page 5). The sentence in 6.2.6.2 should be “... ,of the product of its mass, m_i , (expressed in kilograms), ...”. Delete per square meter two times in 6.2.6.2.

Comment 15: *Observation interval recommendations occurs with two expressions*

In 6.1.2.1.1.3 it says that the condition for the desiccator should be observed both “prior to and following each daily measurement sequence” and “on a regular basis”. Delete “prior to and following each daily measurement sequence”.

Comment 16: *Micrometers in Equation 14*

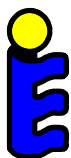
The integration borders have wrong units. It should be micrometers expressed with the Greek “my” and a “m” (μm).

Comment 17: *Change prEn to EN*

Change to EN 12975-1 in Annex B.2.3 instead of prEN 12975-1.

Comment 18: *Rain penetration test*

The rain penetration test has been frequently discussed in the Solar Keymark meetings. The standard has three different methods for detecting rain penetration. It has been concluded that all three different methods are needed in the standard, but they need further specifications. Therefore, have Solar Keymark written three internal papers that address the difficulties and make suggestions how to clearer define all three methods. These papers are suggested to be the Solar Keymark recommendation for revision of the rain penetration test. The papers are added in the Annex 1-3 of this document.



ANNEX 1: Rain Penetration Test, **Weighting the Collector**

Comments and suggestions concerning the rain penetration test defined in 5.7 of EN 12975-2:
5.7.2.2.a: Weighting the Collector

Kostas Voropoulos
NCSR "Demokritos"

Point 1:

The Standard EN 12975-2 suggests three alternative methods of measuring the penetration of water into the collector, after the rain penetration test (5.7.2.2):

- weighting the collector
- humidity measurement
- measuring the condensation level

However, only for the first method it specifies the procedure and the measuring device together with its uncertainty. It says nothing about the other two methods, i.e. the procedure to be followed, instruments, accuracies, e.t.c.

The measurement of humidity inside the collector is a method which introduces many uncertainties due to its nature and it is not mentioned when, how and at which point of the collector this measurement is conducted.

The procedure for the measurement of the condensation level in the inside part of the cover is not also specified. Measuring the area of the condensate is very unreliable since this area does not have regular shapes and is not evenly distributed in the cover.

Our opinion is that the whole procedures for both humidity and condensation level measurements should be mentioned clearly in the test of paragraph 5.7 of EN 12975-2.

Point 2:

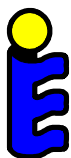
In 5.7.2.2 of EN 12975-2, it is stated that the minimum accuracy of scale must be ± 1 gr for the measurement of the collector weight.

Since there are collectors that their weight can reach over 50 kg, it is obvious that the measurement of such a collector with the accuracy of ± 1 gr presents many uncertainties related to other environmental parameters and requires very expensive balances. It is proposed that the measurement should be conducted with an accuracy of 5 gr/m² collector area.

Point 3:

In the Standard there is no specific mention about the several types of collectors that can be tested in rain penetration, concerning their construction materials. However, there are collectors which have wood on their backs.

Our proposal is that an extra paragraph should be included in 5.7 of the Standard, stating clearly that in cases of collectors having wood in the backs (or other special cases), the laboratory must take all necessary measures so that the final result will not be influenced or altered by the special construction of the collector during the conduction of the test.



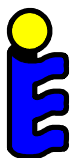
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Comments and suggestions concerning the pass criteria of the rain penetration test defined in 5.3.7 of EN 12975-1

In this paragraph it is stated that the pass criterion for the collector concerning the rain penetration test, and in the case that the weighting method has been used, is that the determined water quantity shall be less than 5 gr/m².

According to our opinion, this figure is too small, since in praxis the majority of the collectors present such water penetration. It should also not be forgotten that actually this is the only test in which a quantitative pass criterion is set, whereas in all other tests it is the "no major failure". This may cause the unhappy situation that a collector with medium efficiency can pass the rain penetration test due to its "heavy sealing", thus being certified and another collector with very high efficiency can be excluded because it did not meet the 5 gr/m² rain penetration criterion.

It is therefore proposed that the acceptance criterion of the rain penetration test for the collector should be 30 gr/m².



ANNEX 2: Rain Penetration Test, Humidity measurements

Comments and suggestions concerning the rain penetration test defined in 5.7 of EN 12975-2:
5.7.2.2.b: Humidity measurements

Christian Müller-Schöll
SPF

As far as I see my job, we are looking for something quantitative, which is still not very easily done, and might need some more experience and also input from other labs, but I will try something that is on the safe side:

For flat plate collectors, an "absolute humidity sensor" has to be placed in the air gap between the absorber and the glazing. Care shall be taken that the sensor does neither touch the glazing nor the absorber. This type of sensor usually consists of two elements, a relative humidity sensor and a temperature sensor. Absolute humidity is assessed by calculation. The collector and the sensor shall be connected to the hot fluid loop for at least five hours before the rain is switched on in order to stabilize. When testing outdoors, in order to minimize disturbances of the measurement, the collector shall be shaded during the whole test.

The humidity shall be monitored from five hours before the raining till at least five hours after the raining.

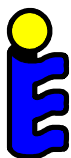
Results

Any visible droplets in the inside of the collector
or a humidity that exceeds 20 g/kg at any time during the periods described above, or a humidity that doubles from the value measured after stabilization during the periods described above, shall yield "major failure" (a mark of "2").

NOTE: Ingress of water might also be detected at a later stage, during the test "Final inspection", Clause 5.11.

Remarks from the author:

We might also need to add a chapter about humidity sensors, calibrations, uncertainties etc. in the appropriate section.
Numerical figures in the text proposed above are subject to discussion.



ANNEX 3: Rain Penetration Test, Measuring of condensation level

Comments and suggestions concerning the rain penetration test defined in 5.7 of EN 12975-2:
5.7.2.2.c: Measuring of condensation level

***Åsa Wahlström, Peter Kovacs and Roger Davidsson,
SP Swedish National Testing and Research Institute***

The Standard EN 12975-2 suggests three alternative methods of measuring the penetration of water into the collector, after the rain penetration test (5.7.2.2):

- weighting the collector
- humidity measurement
- measuring the condensation level

This document gives a suggestion on how to clearer define how the test should be performed when using the *measuring of condensation level* for detection of ingress of water.

Improvements of test method

5.7.2.2

The collector shall be mounted and sprayed as explained above while the absorber in the collector should be kept warm (minimum 50 °C). The heating of the collector shall be started at least 30 minutes before the spraying of water to ensure that the collector box is dry before testing. This shall be done by circulating hot water (or other transfer fluid) above 50 °C through the absorber before but also during the complete test. The option of keeping the absorber warm by exposing the collector to solar radiation are, therefore, not suitable for detection of ingress of water by *measuring the condensation level*.

For the entire time that the test is in progress the absorber is kept warm and this will evaporate the water that finds its way into the collector. The water will thereafter condense on the inside of the glazing, which is being cooled by cold water on the outside. To ensure that no water has penetrated the collector box without forming condensation on the glazing, the collector shall be tipped on all four sides in turn after the test is terminated.

The penetration of water into the collector shall be determined by measuring the condensation level on the cover glass and by measuring the water that come out of the collector when tipping it.

5.7.3

The collector should be sprayed with water at a temperature between 10-25 °C and with a flow rate of approximately 0,05 kg/s per square meter of sprayed area. The duration of the spraying shall be 4 hours.

After 2 hours an intermediate inspection of condensation of the cover glass shall be done in order to facilitate the reporting of the places where water penetrates. After finishing the spraying the inspection of condensation of the cover glass should be done immediately, before the collector will make any temperatures changes. The collector shall not be exposed by solar radiation. The condensation area on the glazing shall be measured.

On completion of the measuring the condensation level, dry the collector carefully on all sides. Tip it on to all four sides in turn, standing it on a clean base on which any water that runs out can be collected and/or approximated quantified.



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5.7.4

The collector should be inspected for water penetration by the presence of any condensation and the approximate quantity of water that leaked out. The results of the inspection i.e. the extension of water penetration and the places where water penetrated shall be reported.

EN 12975-1

5.3.7

c) the measured condensation level shall be less than 5 % of the transparent cover and the collected water shall be less than 20 gr/m².